# Margorejo Underpass Route Choice Study: Reviewed from Traffic Analysis 

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#### Abstract

The signalized intersection at Ahmad Yani street and Margorejo street becomes an intersection with quite long delays at peak hours. street Ahmad Yani is an arterial road that connects Surabaya to Sidoarjo. The presence of high frequency train tracks and a u-turn on the frontage road in front of Giant Maspion Square has resulted in reduced green time on the east side traffic light heading north. One effort to reduce this congestion is to build an underpass. Before an underpass is built, it is necessary to select an underpass route referring to the 1997 Indonesian Road Capacity Manual (MKJI). The results obtained in this final assignment are the determination of the Margorejo-Ahmad Yani route which is recommended for an underpass to be built because the large delay that occurs is 687 sec/smp on Jalan Ahmad Yani Sidoarjo-Surabaya; 1938 det/smp on Jalan Ahmad Yani Surabaya- Sidoarjo; $149 \mathrm{sec} / \mathrm{smp}$ on Jalan Margorejo; and 120 on the frontage road. The DS that occurred was 1.33 on Jalan Ahmad Yani Sidoarjo-Surabaya; 1.66 on Jalan Ahmad Yani Surabaya-Sidoarjo; 0.9 on Jalan Margorejo; and 0.22 on road frontage. The queue length was 648 secondary schools on Jalan Ahmad Yani Sidoarjo-Surabaya; 2422 junior high schools on Jalan Ahmad Yani Surabaya-Sidoarjo; 68 junior high school on Jalan Margorejo; and 18 junior high schools on the frontage road. With the construction of the Margorejo underpass, the DS on all sections will be 1,074 on Jalan Ahmad Yani Sidoarjo-Surabaya; 1,385 on Jalan Ahmad Yani Surabaya-Sidoarjo; 0.5 on Jalan Margorejo; and 0.07 on road frontage. Delays and long queues no longer exist because there are no longer traffic lights.


Keywords- Route Selection Study, Underpass, Margorejo, Surabaya, Traffic Analysis.

## I. INTRODUCTION

## A. BACKGROUND

Street Ahmad Yani is one of the access roads that connects the city of Surabaya with the city of Sidoarjo. This road is an arterial road. In fact, the road that connects Surabaya and Sidoarjo is not only Jalan Ahmad Yani, but there is also the Middle East Ring Road (MERR), the Outer East Ring Road (OERR) which is still in the planning process, and via the Raya Rungkut-Jalan Rungkut Menanggal road. It's just that there are still many people who pass through Jalan Ahmad Yani to go to Sidoarjo because it is closer to the middle of Surabaya city and the middle of Sidoarjo city, besides the road is also wider. The large number of vehicles passing through this road causes traffic jams at each sidepeak hour. The bottleneck on the north side that leads to the south lies in the entrance to frontage road and the intersection of Jalan Ahmad Yani with Jalan Margorejo. The traffic jam on the south to north side is located only at the intersection of Jalan Ahmad Yani and Jalan Margorejo.

Red time which is quite long and the implementation of only one LTOR results in a long period of time to reduce the density on the road. The only traffic jam on the east side is at the intersection of Jalan Margorejo and Jalan Ahmad Yani.Red time is quite long, and the presence of high frequency train crossings results in a long breakdown of traffic jams, especially whenpeak hour.

This problem needs to be overcome by building an underpass as an alternative to reduce congestion. In evaluating the construction of an underpass to overcome congestion at the

[^0]Margorejo-Ahmad Yani intersection, traffic analysis is needed. This traffic analysis is needed to determine the route that will be chosen as the location for the underpass construction. The stages of route selection analysis using traffic analysis are presented in Figure 1.

## II. METHODOLOGY

The research flow diagram is displayed in Figure 2.

## III. DISCUSSION

## A. TRAFFIC ANALYSIS AT AHMAD YANI INTERSECTION-EXISTING MARGOREJO

Determining the condition of the existing intersection is carried out through several levels, that is calculation degrees saturation, stop rate, delay, and interweaving.

1. Degrees Saturation (Degree of Saturation)

To calculate the degree of saturation, traffic volume data obtained from the results is needed traffic counting moment peak hour.
a) Passenger Car Equivalence Calculation

For passenger car equivalent calculations, use a multiplier of 1 for LV emp; 1.2 for HV emp; 0.2 for emp MC. Complete calculation results can be seen in Table 1.
b) Calculation of Signalized Intersection Capacity (C) In this analysis, the following data is known.
Path width $=10.5$ meters.
$S 0=10,5 \times 600=10,5 \times 600=6300$
Correction factor:
$\mathrm{F} 1=\mathrm{FCS}=1$
$\mathrm{F} 2=\mathrm{FSF}=0,8 \mathrm{~F} 3=\mathrm{FG}=1$
$\mathrm{F} 4=\mathrm{FP}=$ none
$\mathrm{F} 5=\mathrm{FRT}=1+p L T \times 0,26=1+0,47 \times 0,26=1,1215$
$\mathrm{F} 6=\mathrm{FLT}=1+p R T \times 0,26=1-0,08801 \times 0,16=0,9859$
$S=6300 \times 1 \times 0,83 \times 1 \times 1,1215 \times 0,9859=5799$


Fig 1. Methodology Election Route Underpasses
$\mathrm{g}=45$ seconds and $\mathrm{c}=227$ seconds

$$
C=S \times \frac{g}{c}=5799 \times \frac{45}{227}=1146
$$

c) Calculation of Degree of Saturation

After getting the capacity in the calculation above, then calculate the degree of saturation using formula (6):

$$
D S=\frac{Q}{C}=\frac{1034}{1146.1}=0.9022
$$

2. Calculation of Queue Length

After getting the degree of saturation, the next step is to calculate the queue length.

$$
\begin{aligned}
& N Q 1=0,25 \times C X\left[(D S-1)+\sqrt{(D S-1)+\frac{8 x(D S-0,5)}{C}}\right] \\
& =0,25 \times 1146,1 \times\left[(0,9022-1)+\sqrt{(0,9022-1)+\frac{8 x(0,9022-0,5)}{1146,1}}\right] \\
& =3,85 \\
& N Q 2=c \times \frac{1-G R}{1-G R \times D S} \times \frac{Q}{3600} \\
& =227 \times \frac{1-0,1982}{1-0,1982 \times 0,9022} \times \frac{1034}{3600}=63,66
\end{aligned}
$$

TABLE 1.
Passenger Car Equivalence Calculation for Ahmad YaniMargorejo intersection

| Approach | LV |  | HV |  | MC |  | total MV |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | vehicl <br> e | emp | vehic <br> le | emp | vehicle | emp | vehicle | emp |
| S | 3132 | 3132 | 30 | 39 | 5529 | 1107 | 8691 | 2852 |
| N | 3046 | 3046 | 54 | 72 | 10259 | 2053 | 17508 | 5171 |
| AND | 575 | 575 | 0 | 0 | 2288 | 459 | 2863 | 1034 |
| EC | 316 | 316 | 0 | 0 | 174 | 61 | 614 | 342 |

TABLE 2.
Intersection Analysis Calculation Table Before Adding Train

| Passing Time (1) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\substack{\text { Appro } \\ \text { ach }}}$ | $\underbrace{}_{\substack{\text { Approach } \\ \text { widu } \\ \text { (wee }}}$ | so |  | $\underbrace{}_{\substack{\text { Side } \\ \text { onstactes } \\(\text { (sf) }}}$ |  |  | $\begin{aligned} & \text { Tum } \\ & \text { (lunt } \\ & \text { (fitit } \end{aligned}$ | $s$ |
| $\begin{aligned} & \text { S } \\ & \text { IN } \\ & \text { T } \\ & \hline \end{aligned}$ | $\begin{aligned} & 7 \\ & 10,5 \\ & 10,5 \\ & 10, \\ & \hline \end{aligned}$ | $\begin{aligned} & 4200 \\ & 6.300 \\ & 6.300 \\ & 48800 \end{aligned}$ |  | $\begin{aligned} & 0.95 \\ & 0.95 \\ & 0.053 \\ & 0.9275 \end{aligned}$ | 1 1 1 1 1 | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 1,12 \\ & 1,13 \end{aligned}$ | 0 0 0.97 0.09 0.98 | $\begin{gathered} 3990 \\ \hline 7999 \\ \hline 77.19 \\ \hline 495.93 \\ \hline \end{gathered}$ |

TABLE 3.
Intersection Analysis Calculation Table Before Adding Train Passing Time (2)

| Approa <br> ch | g | c | C | DS | GR | NQ1 | NQ2 | $\begin{aligned} & \hline \text { NQ1+ } \\ & \text { NQ2 } \\ & \hline \end{aligned}$ | NQ max |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S | 122 | 227 | 2144,41 | 1,33 | 0,54 | 357 | 292 | 648 | 858,1318 |
| u | 122 | 227 | 3116,64 | 1,66 | 0,54 | 1029 | 1393 | 2422 | 3199,376 |
| T | 45 | 227 | 1146,11 | 0,90 | 0,20 | 4 | 64 | 68 | 91,94952 |
| TL | 51 | 227 | 1115,49 | 0,31 | 0,22 | 0 | 18 | 18 | 26,54311 |

TABLE 4.
Table Calculation Analysis Intersection Before Added Train Passing Time (3)

| Approach | QL | NS | Nsv | psv | DT | PT | DG | D |
| :--- | ---: | :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| S | 2451,81 | 3,24 | 9248,25 | 1 | 683,29 | 0 | 4 | 687,2873 |
| U | 6094,05 | 6,68 | 34564,06 | 1 | 1933,84 | 0,31 | 4 | 1937,842 |
| T | 175,14 | 0,93 | 963,54 | 0,93 | 144,87 | 1 | 4,14 | 149,0097 |
| TL | 66,36 | 0,75 | 256,30 | 0,75 | 115,74 | 1 | 4,50 | 120,2447 |

$\mathrm{NQ}=\mathrm{NQ} 1+\mathrm{NQ} 2=4+64=68 \mathrm{smp}$
The graph in MKJI shows the average NQ value is 50 pcu , whereas in this analysis, the average NQ is 68 pcu. Therefore, manual calculations using Excel are needed, taking $\mathrm{pOL}=1 \%$, then the NQ max value obtained for this study is:
$\mathrm{NQmax}=1,4255 \times 68+4,3=101 \mathrm{smp}$
$Q L=\frac{N Q \max \times 20}{W \text { etnters }}=\frac{91,95 \times 20}{10,5}=175,14$

## 3. Stop Number Calculation

After calculating the queue length, the next step is to calculate the stopping number.
$N S=0,9 \times \frac{N Q}{Q \times c} \times 3600$
$N S=0,9 \times \frac{67,507}{1034 \times 227} \times 3600=0,93=1$ Stop $/$ hour
Nsv $=1034 \times 1,9319=963,54 \mathrm{pcu} /$ hour

## 4. Delay Calculation

After calculating the stopped vehicle, the next step is to

TABLE 5.
Passenger Car Equivalence Calculation for Ahmad YaniMargorejo intersection

| approach | Wide approach <br> (We) | So | size city <br> (Fcs) | Obstacle side <br> (Fsf) | Kelan daian <br> (Fg) | Turn right <br> (Frt) | Turn left <br> (Flt) | S |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S | 7 | 4200 | 1 | 0.95 | 1 | 0 | 0 | 3990 |
| U | 10.5 | 6300 | 1 | 0.95 | 1 | 0 | 0.97 | 5799 |
| Q | 10.5 | 6300 | 1 | 0.95 | 1 | 1.12 | 0.99 | 6617.37 |
| TL | 6.5 | 3900 | 1 | 0.93 | 1 | 1.13 | 0.98 | 4034.09 |

TABLE 6.
Intersection Analysis Calculation Table Before Adding Train Passing Time (1)

| appro <br> ach | g | c | C | DS | GR | NQ1 | NQ2 | NQ1+ <br> NQ2 | NQ <br> max |
| :--- | :--- | :--- | :--- | :--- | :--- | ---: | :--- | ---: | ---: |
| S | 232 | 337 | 2746.83 | 1.04 | 0.69 | 65 | 292 | 356 | 512 |
| U | 232 | 337 | 3992.2 | 1.30 | 0.69 | 593 | 1393 | 1985 | 2384 |
| Q | 45 | 337 | 787.93 | 1.31 | 0.13 | 79 | 100 | 178 | 259 |
| TL | 51 | 227 | 906.34 | 0.38 | 0.22 | 1 | 30 | 30 | 47 |

TABLE 7.
Intersection Analysis Calculation Table Before Adding Train Passing Time (2)

|  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| approach | QL | NS | Nsv | psv | DT | PT | DG | D |
| S | 1349,88 | 1,20 | 3420,47 | 1 | 141,39 | 0 | 4 | 145,39 |
| U | 4995,69 | 3,69 | 19082,06 | 1 | 1352,45 | 0,31 | 4 | 1356,45 |
| T | 453,81 | 1,66 | 1714,6 | 1 | 517,75 | 0,09 | 4 | 521,75 |
| TL | 140,69 | 0,84 | 286,73 | 0,76 | 180,7 | 1 | 4,48 | 185,02 |

TABLE 8.
Table Calculation Analysis Intersection Before Added Train Passing Time (3)

| Margorejo segment |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time |  |  |  | Margorejoroyal | Margorejoayani | Margorejofrontage | Total |
| 16 | 0 | 17 | 0 | 1155 | 107 | 88 | 1350 |
|  | 15 |  | 15 | 1176 | 99 | 90 | 1365 |
|  | 30 |  | 30 | 1265 | 110 | 91 | 1466 |
|  | 45 |  | 45 | 1333 | 122 | 92 | 1547 |
|  |  |  |  |  |  | TOTAL | 5728 |

calculate the delay.
$D T=c x \frac{0,5 x(1-G R)^{2}}{(1-G R x D S)}+\frac{N Q 1 \times 3600}{C}$
$D T=202 x \frac{0,5 x(1-0,1982)^{2}}{(1-0,1982 x 0,9022)}+\frac{3,8474 \times 3600}{1146,1}$
$D T=144,87 \mathrm{sec} / \mathrm{pcu}$
Psv $=\min (N S, 1)=1$ karenaNS $<1$, makadiambil
$N S=0,9319$
$D G=(1-P s v) x P t x 6+(P s v x 4)$
$D G=(1-1) x 0,9319 \times 6+(1 x 4)=3 \mathrm{sec} / p c u$
$D=D T+D G=114,0937+4=118,0937 \mathrm{sec} / \mathrm{pcu}$
5. Braided

After count analysis intersection, then the next step is to calculate the braid. To calculate PHF (Peak Hour Factor), enter the data in Table 5.9 into formula (16).


Fig 2. Method Processing


Fig 3. Method Processing

$$
P H F=\frac{5728}{4 \times 1547}=0,9257
$$

Is known:
$\mathrm{Er}=1.5$ (for flat roads) in table 2.8
$\mathrm{Fp}=1$ (assuming the driver is familiar with the road)

$$
\begin{aligned}
& f H V-r=\frac{1}{1+1(1-1)}=1 \\
& V r=\frac{371}{0,9257 \times 1 \times 1}=400,794 \mathrm{pcu} / \mathrm{hour} \\
& f H V-f=\frac{1}{1+1(1-1)}=1 \\
& V f=\frac{1135}{0,9257 \times 1 \times 1}=1226,1587 \mathrm{pcu} / \mathrm{hour}
\end{aligned}
$$

$$
\mathrm{P}_{\mathrm{FM}}=0,5775+0,000028 \times \mathrm{L}
$$

$$
=0,5775+0,000028 \times 171,2598
$$

$$
=0,5823
$$

$$
\mathrm{V}_{12}=\mathrm{vf}_{\mathrm{f}} \times \mathrm{P}_{\mathrm{FM}}=1226,1587 \times 0,5823=713,98 \mathrm{pc} / \mathrm{h}
$$

$$
\mathrm{VFO}_{\mathrm{FO}}=\mathrm{Vf}_{\mathrm{f}}+\mathrm{v}_{\mathrm{r}}=1226,1587+400,794=1626,9427 \mathrm{pc} / \mathrm{h}
$$

TABLE 9.
Results of Passenger Car Equivalence Calculations for Interwebs

|  |  | MC | LV | MC | LV | total |
| ---: | :--- | ---: | ---: | ---: | ---: | ---: |
| 1a | margorejo-ayani | 55 | 80 | 11 | 80 | 91 |
| 1b | margorejo-frontage | 169 | 44 | 34 | 44 | 78 |
| 2 | margorejo royal/2 | 1166 | 249 | 234 | 249 | 483 |
| 3a | margorejo-royal/2 | 1166 | 249 | 234 | 249 | 483 |
| 3b | frontage-royal | 202 | 290 | 81 | 290 | 371 |

TABLE 10.
Passenger Car Equivalence Calculation for the Ahmad Yani-Margorejo Section

| App roac h | LV |  |  | H.V |  |  | vic |  |  | Q |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | total | $\begin{aligned} & \text { corium } \\ & \hline \text { noll } \end{aligned}$ | emp | total | $\begin{aligned} & \hline \text { colum } \\ & \text { nol } \end{aligned}$ | emp | total | $\begin{aligned} & \text { čerum } \\ & \text { cher } \end{aligned}$ | emp |  |
| 3 | गड0 | 1044 | 1044 | 50 | 10 | 12 | כ29 | 1845 | 401 | 171 |
| N | 3150 | 1050 | 1050 | 5 | 17 | 21 | 10011 | 5531 | 885 | $1{ }^{1}$ |
| AND | 788 | 394 | 394 | 0 | 0 | 0 | 2534 | 126/ | 311 | 711 |
| EC | 124 | 42 | 42 | 0 | 0 | 0 | 100 | 250 | 59 | 101 |

TABLE 11.
Free Flow Speed Calculation Results

| Approach | FvO | FVIn | FFVSF 6 | FFVCS | FV |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 61 | 0 | 0,896 | 1 | 54,66 |
| N | 61 | 0 | 0,896 | 1 | 54,66 |
| AND | 61 | 0 | 0,896 | 1 | 54,66 |
| EC | 61 | 0 | 0,896 | 1 | 54,66 |

TABLE 12
Results of Calculation of Degree of Saturation

| Appro <br> ach | FCIn | FCSP | FCSF <br> 6 | FCCS | C | DS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S | 1 | 1 | 0,856 | 1 | 1412,4 | 1,074 |
| N | 1 | 1 | 0,566 | 1 | 1414,4 | 1,385 |
| AND | 1 | 1 | 0,556 | 1 | 1412,4 | 0,503 |
| EC | 1 | 1 | 0,856 | 1 | 1412,4 | 0,072 |

The maximum capacity of a 3-lane freeway at a speed of 40 $\mathrm{km} / \mathrm{h}$ (or about $24.8 \mathrm{miles} / \mathrm{h}$ ) is $5345.6425 \mathrm{pc} / \mathrm{h}$. Because $1626.9427 \mathrm{pc} / \mathrm{h}<5345.6425 \mathrm{pc} / \mathrm{h}$, the freeway is still considered feasible.
Genre total Which enters in areas merge calculated:
$\mathrm{v}_{\mathrm{r} 12}=\mathrm{v}_{\mathrm{r}}+\mathrm{v}_{12}=400,794+713.98=1114.7746 \mathrm{pc} / \mathrm{h}$
The maximum capacity of a single-lane ramp at a speed of $20 \mathrm{~km} / \mathrm{h}$ (or about 12.47 miles $/ \mathrm{h}$ ) is $1800 \mathrm{pc} / \mathrm{h}$. Because 1114.7746 $\mathrm{pc} / \mathrm{h}<1800 \mathrm{pc} / \mathrm{h}$ so ramps still said to be feasible.
$\mathrm{D}_{\mathrm{R}}=5,475+0.00743 \times \mathrm{v} \mathrm{r}++0.0078 \times \mathrm{v} 12-0.00627 \times \mathrm{L} \mathrm{a}$
$=5,475+0.00743 \times 400,794+0.0078 \times 715.64767-0.0067 \times$
$171.2598=2.4136 \mathrm{pc} / \mathrm{m} / \mathrm{ln}$
Because $D_{R}=2.4136=0-10$ then it includes level of service A in the merging area.
$M_{S}=0.321+0.0039 x e^{(v r 12 / 1000)}-0.002 x\left(\frac{L a x R F F S}{1000}\right)$
$=0.321+0.0039 \times e^{1.1115}-0.002 x\left(\frac{171.2598 \times 20}{1000}\right)$


Fig 4. Method Processing with figure 2.
$=0,33$
$\mathrm{Sr} \quad=\mathrm{FFS}-($ FFS -42$) \times \mathrm{M} \mathrm{s}$
$=40-(40-42) \times 0.3361$
$=40.66 \mathrm{~km} / \mathrm{h}$
$V_{0 a}=\frac{\left(V_{f}-V_{12}\right)}{N_{0}}=\frac{(1226,15-1114,7746)}{1}$
$=111,374 \mathrm{pc} / \mathrm{h}$
Because V oa $=111,374<500$ so in Table 2.8 use formula (27) And (30).
$S_{0}=F F S=40 \mathrm{~km} / \mathrm{h}$
$S=\frac{1114,7746+111,374 \times 1}{\left(\frac{1114,7746}{40,66}\right)+\left(\frac{111,374}{40}\right)}=40,6 \mathrm{~km} / \mathrm{h}$

## B. Analysis Cost Operational Vehicle

After the DS (Degree of Saturation) data, queue length, vehicle stops and total delays are obtained, analysis is then carried out to determine operational costs. vehicle on intersection on condition existing based on the Highway Engineering book.

For the calculation example below, a road section is taken Margorejo, like on example on. After field survey and get an approaching speed of $35 \mathrm{~km} / \mathrm{h}$, which can be seen in Figure 3.1.

With DS $=0.9022$ And speed plan Margorejo road is $40 \mathrm{~km} / \mathrm{h}$, from the graph above we get:

1. Cost walks straight $=71$ dollars $/ 1000$ vehicle miles $=$ 509,291 rupiah/km vehicle
2. Time journey $=35.5$ hours $/ 1000$ miles vehicle $=79.4$ sec/km vehicle
3. Speed walk average $=27.5$ miles $/ \mathrm{h}=44.26 \mathrm{~km} / \mathrm{h}$
4. Additional speed change fee $=4.8$ dollars $/ 1000$ miles $=$ 34.43092 rupiah $/ \mathrm{km}$ miles

With speed approach intersection $\pm 25 \mathrm{~km} / \mathrm{h}=15.5 \mathrm{miles} / \mathrm{h}$ and speed stay away intersection $\pm 40 \mathrm{~km} / \mathrm{h}=24.9$ mile $/ \mathrm{h}$, from chart found:

1. Cost transition speed $=1.5$ dollars $/ 1000$ passenger vehicles $=17.32$ rupiah $/ 1000$ vehicles
From the graph we get:
2. Average stop per vehicle $=0.95$ per signal
3. Additional stopping delay $=3.2$ hours $/ 1000$ vehicles/signal = 11.52 seconds/vehicle/signal.
4. Additional stopping fee $=13$ dollars running fee/ 1000 vehicles/signal $=150.07$ rupiah walking fee/vehicle/signal
With DS $=0.9022$ And C $=1146.1$, so from graph obtained:
5. Slowness average per vehicle $=46$ second
6. Idle time $=12.85$ hours $/ 1000$ vehicles $=46.26$ seconds/vehicle
7. Dwelling fee $=3.2$ dollars/1000 passenger vehicles $=$ 36,941 rupiah/passenger vehicle
So that total time and total cost for a passenger vehicle at the intersection on Jalan Margorejo:
Total time $=$ time journey + addition slowness stops + slowness average per vehicle + dwell time + average delay
Total time $=79.4+11.52+9.72+46+46.26=332.2$ second
Total cost $=$ cost of going straight + additional cost of changing speed + cost of changing speed + additional cost of stopping + additional cost of stopping
Total cost $=509,291+34.43092+17,316+150.07+36,941$

$$
\text { = } 748 \text { rupiah }
$$

All calculations above are based on DS. Meanwhile, if the calculation above was based on approaching speed, the results would be different. The differences are as follows:

1. Travel time $=40$ hours $/ 1000$ vehicle miles $=89.48$ seconds/vehicle km
2. Additional stopping delay $=2.7$ hours/ 1000 vehicle miles $=9.72$ seconds/vehicle km
3. Additional stopping fee $=9.1$ dollars running fee/1000 vehicles/signal $=105.05$ rupiah walking fee/vehicle/signal
So that total cost based on approach speed $=703.3$ rupiah and total time $=257.2$ seconds.

All calculations on multiplied coefficient the truck multiplier is 1.00 because the percentage of single unit trucks is $0 \%$ and the percentage of $3-\mathrm{S} 2$ combination diesel trucks is $0 \%$. It can be seen in tables 2.13 and 2.14 that the adjustment factor for the percent of trucks due to staying in the traffic flow (time) is 1 and the adjustment factor for the percent of trucks due to staying in the traffic flow (cost) is 1.

For table results calculation in full can be seen in the attachment.

## C. Analysis Cost Operational Vehicle

After determining the underpass route, then next a traffic analysis was carried out for the Ahmad Yani-Margorejo section to determine the degree of saturation. In this calculation, the example of the Margorejo section is taken.

1. Passenger Car Equivalence Calculation

For passenger car equivalence calculations, use a multiplier coefficient of 1 for emp LV; 1.2 for HV emp; 0.25 for emp MC. Complete calculations can be seen in Table 3.10.
2. Free Flow Speed Analysis

After calculating the equivalence, the next step is to calculate the free flow velocity analysis using formula (31) is known:
$\mathrm{FV}_{0} \quad=61$ (because of the six-lane-divided road type with vehicle LV)
FVw $=0$ (because the road type is four-lane-divided, and the
lane width is 3.5 meters).
FFV ${ }_{\text {SF }}=0.896$ (because of the four-lane-divided road type, high side resistance class, with a shoulder width of 0.5 and after being multiplied by the free flow speed adjustment factor for six-lane roads).
FFV ${ }_{C S}=1$ (because the population of the city of Surabaya is 2,815,603 people).
Then enter it into the free flow velocity formula, as below:
$F V=(61+0) \times 0.896 \times 1=54,656 \mathrm{~km} / \mathrm{h}$
For free flow speed calculation results, you can see table 3.11.
3. Capacity Calculation

After calculating the free flow speed, the next step is to calculate the road capacity using formula (33) is known:
$\mathrm{Co}=1650$
FCIN=1
FCSP = 1
FCSF $=0,82$
FCCS $=1$
Then enter it into the capacity formula, as below:
$C=1650 \times 1 \times 1 \times 0.82 \times 1=1412.4$
4. Degrees Saturation

After count capacity, so Next, calculate the degree of saturation.

$$
D S=\frac{711}{1412,4}=0,5034
$$

For results calculation can be seen on table 3.12.

## D. Picture Geometric Underpasses

After analyzing Then cross after There is underpass, then next draw the geometric underpass.

Is known:
Point A = 471443,4737; - 793162,717
Point $B=471401.5977 ;-792007,178$
Point C = 472704.3962; - 792015,714
$\alpha=\arctan \left(\frac{471401.5977-471443,4737}{-792007,178-(-793162,717)}\right)=357,92$
$\beta=\arctan \left(\frac{472704.3962-471401.5977}{-792015,714-(-792007,178)}\right)=90,38$
$\Delta=\arctan (357,92-90,38)=92,45$
Planned:

1. $\mathrm{V}=40 \mathrm{~km} / \mathrm{h}$
2. $\mathrm{e} \max =10 \%$
3. $R=477$ meters.

$$
\begin{aligned}
& \mathrm{f} \max =-0.00065 \times 40+0.192=0.166 \\
& \operatorname{Rmin}=\frac{40^{2}}{(127 \times(10 \%+0,166))}=47,36 \text { meters } \\
& \operatorname{Dmax}=\frac{1432,4}{47,36}=30,24 \\
& D=\frac{1432,4}{477}=3 \\
& e=\left(-\left(\frac{10 \%}{30,24}\right)\right) \times D^{2}+\left(\frac{2 \times 10 \%}{30,24}\right) \times 3=1,89 \%
\end{aligned}
$$

Because $\mathrm{e}=1.89 \%$ And not enough from 3\%, so corners including full circles. Next, the calculation is carried out:

$$
\begin{aligned}
& T c=477 \times \operatorname{tg}\left(\frac{1}{2} x 92,45\right)=497,85 \text { meters } \\
& E=\frac{477}{\cos \left(\frac{1}{2} x 92,45\right)}-477=212,48 \text { meters } \\
& T c=\left(\frac{92,45 \times \pi}{180}\right) \times 477=769,67 \text { meters }
\end{aligned}
$$

By using a guard depth of 3 meters, tall room underpass 5 meters, and slope $5 \%$, then the horizontal slope distance is 299 meters.

## IV. CONCLUSION AND RECOMMENDATIONS

## 1. Conclusion

This final project is an evaluation of the performance of the Ahmad Yani-Margorejo intersection if an underpass is built. The Ahmad Yani-Margorejo intersection is a signalized 3 intersection with 4 phases, which are long cycle time is 227 seconds. From the results of the analysis, the following conclusions were obtained.

1) The current performance of the Ahmad YaniMargorejo intersection shows:
a. The largest traffic flow is the North (N) approach, namely $5335 \mathrm{pcu} /$ hour and the smallest are the Northeast (TL) approach, namely $673 \mathrm{pcu} /$ hour.
b. The degree of saturation for each approach is 1.33; 1.66; 0.9; and 0.4 for the South, North, East, and Northeast approaches.
c. The delay that occurred was $687 ; 1938 ; 149$; and 123 seconds for the South, North, East, and Northeast approaches.
d. Total time on each approach is 926.0172; 2173,871; 332,2009 ; and 240.3873 .
seconds for the South, North, East, and Northeast approaches.
e. The total cost for each approach is 758.91; 728.89; 748.05 ; and 788.45 rupiah for the South, North, East and Northeast approaches.
The values for the degree of saturation and delay are the values without including additional red time for the East (Margorejo) and Northeast (Frontage Road) approaches when trains pass. Meanwhile, the value of the degree of saturation and delay with the addition of the train variable is.
a. The degree of saturation at each approach is 1.038; 1,$295 ; 1.17$; and 0.56 for the South, North, East, and Northeast approaches.
b. The delay on each approach is $145.39 ; 1356.45 ; 521.75$; and 185.02 seconds for the South, North, East and Northeast approaches.
c. Total time on each approach is $384.115 ; 1592,476$; 757.7788; and 239.4831 seconds for the South, North, East, and Northeast approaches.
d. The total cost for each approach is 758.91; 728.89; 728.89; and 788.45 rupiah for the South, North, East and Northeast approaches.
2) From the results of the performance analysis in conclusion number 1, the route choice is determined underpass is route 3, namely Margorejo-Ahmad Yani, because route 3 can eliminate everything traffic light and nothing crash by railroad. Meanwhile, the distance between the mouth underpass with flyover Wonokromo on route 3 is the longest, namely 765 meters.
3) By selecting route 3 for underpass, it is obtained that the intersection performance becomes the section performance because there is no conflict between vehicles. The existing intersection performance is:
a. The degree of saturation at each approach is 1.075; 1,$385 ; 0.336$; and 0.072 for the South, North, East, and Northeast approaches.
b. The braid capacity is still said to be feasible because of the capacity freeway (INFO) $1626.9427 \mathrm{pc} / \mathrm{h}$ smaller maximum capacity is $5345.6425 \mathrm{pc} / \mathrm{h}$ and capacity ramp (INR12) $1114.7746 \mathrm{pc} / \mathrm{h}$ is smaller than the maximum capacity of $1800 \mathrm{pc} / \mathrm{h}$. Level of service (LOS) A due to average density (DR) 2.4136, entered in the 0-10 scale for LOS A.

## 2. Suggestion

The analysis in this final project provides an overview of the performance improvement at the Ahmad Yani-Margorejo intersection. In this analysis there are still important things that need to be analyzed more deeply regarding design underpass. The analysis required is determining depth underpass related to the high frequency of train crossings. This depth is necessary to avoid the influence of vibrations on the building structure underpass. The depth obtained will influence the geometric design underpass.

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